## KH600

## 1GHz, Differential Input/Output Amplifier

## Features

- DC - 1 GHz bandwidth
- Fixed $14 \mathrm{~dB}(5 \mathrm{~V} / \mathrm{V})$ gain
- $100 \Omega$ (differential) inputs and outputs
- $-74 /-64 \mathrm{dBc} 2 \mathrm{nd} / 3 \mathrm{rd} \mathrm{HD}$ at 50 MHz
- 45 mA output current
- $9 \mathrm{~V}_{\mathrm{pp}}$ into $100 \Omega$ differential load
- $13,000 \mathrm{~V} / \mu \mathrm{s}$ slew rate
- Optional supply current and offset voltage adjustment


## Applications

- ATE systems
- High-end instrumentation
- High bandwidth output amplifier
- Differential buffer
- Line driver


## Typical Application



The KH600 includes $50 \Omega$ resistors from each input to ground (resulting in a differential input impedance of $100 \Omega$ ).



## Pin Assignments



NOTE: Case is grounded.

## Pin Definitions

| Pin Number | Pin Name | Pin Function Description |
| :---: | :---: | :--- |
| 6,10 | $+\mathrm{V}_{\mathrm{S}}$ | Positive supply voltage |
| 8 | $-\mathrm{V}_{\mathrm{S}}$ | Negative supply voltage |
| 11 | $+\mathrm{V}_{\mathrm{b} 1}$ | Positive bias voltage for OUT1 |
| 5 | $+\mathrm{V}_{\mathrm{b} 2}$ | Positive bias voltage for OUT2 |
| 2 | $-\mathrm{V}_{\mathrm{b}}$ | Negative bias voltage for OUT1 and OUT2 |
| 1 | IN1 | Input 1, +IN |
| 3 | IN2 | Input 2, -IN |
| 9 | OUT1 | Output 1, +OUT |
| 7 | OUT2 | Output 2, -OUT |
| 4,12 | GND | Input termination ground and case |

## Absolute Maximum Ratings

| Parameter | Min. | Max. | Unit |
| :--- | :---: | :---: | :---: |
| Total Supply Voltage | - | 15 | V |
| Maximum Junction Temperature | - | +150 | ${ }^{\circ} \mathrm{C}$ |
| Storage Temperature Range | -65 | +150 | ${ }^{\circ} \mathrm{C}$ |
| Lead Temperature, 10 seconds | - | +300 | ${ }^{\circ} \mathrm{C}$ |

## Electrical Specifications

$\left(G=+5 \mathrm{~V} / \mathrm{V}(14 \mathrm{~dB}), \mathrm{R}_{\mathrm{L}}=100 \Omega\right.$ (differential), $\mathrm{T}_{\mathrm{a}}=+25^{\circ} \mathrm{C},+\mathrm{V}_{\mathrm{b} 1}=+\mathrm{V}_{\mathrm{b} 2}=+\mathrm{V}_{\mathrm{S}}=+5 \mathrm{~V},-\mathrm{V}_{\mathrm{b}}=-\mathrm{V}_{\mathrm{S}}=-5 \mathrm{~V}$; unless noted)

| Parameter | Conditions | Min. | Typ. | Max. | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Frequency Domain Response |  |  |  |  |  |
| -3dB Bandwidth | $\mathrm{V}_{0}=2 \mathrm{~V}_{\mathrm{pp}}$ |  | 1000 |  | MHz |
| Peaking | DC to 250MHz |  | 0.2 |  | dB |
|  | DC to 500 MHz |  | 0.5 |  | dB |
| Full Power Bandwidth | $\mathrm{V}_{0}=8 \mathrm{~V} \mathrm{pp}$ |  | 350 |  | MHz |
| Linear Phase Deviation | DC to 500 MHz |  | 3 |  | deg |
| Gain | 1 MHz |  | 14 |  | dB |
|  | DC ${ }^{1}$ | 14.2 | 14.3 | 14.4 | dB |
| Input Return Loss (SE 50, ${ }^{2}$ | DC $=250 \mathrm{MHz}$ |  | 22 |  | dB |
|  | DC $=500 \mathrm{MHz}$ |  | 14 |  | dB |
| Output Return Loss (SE $50 \Omega$ ) ${ }^{2}$ | DC $=500 \mathrm{MHz}$ |  | 27 |  | dB |
| Time Domain Response |  |  |  |  |  |
| Rise and Fall Time | 2 V step |  | 350 |  | ps |
|  | 8 V step |  | 1 |  | ns |
| Overload Recovery | $\mathrm{V}_{\text {in }}=4 \mathrm{~V}_{\mathrm{pp}}$ |  | 900 |  | ps |
| Slew Rate | 8 V step |  | 13,000 |  | V/us |
| Distortion and Noise Response |  |  |  |  |  |
| 2nd Harmonic Distortion | 5 V pp, 50 MHz |  | 61 |  | dBc |
|  | $2 \mathrm{Vpp}, 50 \mathrm{MHz}{ }^{1}$ | 61 | 74 |  | dBc |
|  | 1 V pp, 200MHz |  | 65 |  | dBc |
| 3rd Harmonic Distortion | 5 V pp, 50 MHz |  | 46 |  | dBc |
|  | $2 \mathrm{~V}_{\mathrm{pp}}, 50 \mathrm{MHz}{ }^{1}$ | 57 | 64 |  | dBc |
|  | 1 V pp, 200MHz |  | 70 |  | dBc |
| Input Referred Noise | $>1 \mathrm{MHz}$ |  | 1.35 |  | $\mathrm{nV} / \mathrm{NHz}$ |
| Noise Figure |  |  | 6.5 |  | dB |
| DC Performance |  |  |  |  |  |
| Output Offset Voltage | I/Os terminated $50 \Omega$ to GND ${ }^{1}$ | -60 | -18 | +60 | mV |
| Average Drift |  |  | 200 |  | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Power Supply Rejection Ratio ( $\pm \mathrm{V}_{\mathrm{S}}$ ) | DC |  | 55 |  | dB |
| Supply Current | $\pm \mathrm{V}_{\text {s }}$ pins $^{1}$ |  | 67 | 70 | mA |
|  | $\begin{aligned} & \pm \mathrm{V}_{\mathrm{b}} \text { pins } \\ & \left(+\mathrm{V}_{\mathrm{b} 1} \text { shorted to }+\mathrm{V}_{\mathrm{b} 2}\right)^{1} \end{aligned}$ |  | 22 | 24 | mA |
| Output Characteristics |  |  |  |  |  |
| Output Voltage Swing | differential |  | 9 |  | $\mathrm{V}_{\mathrm{pp}}$ |
| Output Current |  |  | $\pm 45$ |  | mA |
| Recommended Operating Conditions |  |  |  |  |  |
| Total Supply Voltage | $\left(+\mathrm{V}_{\mathrm{S}}\right.$ to $\left.-\mathrm{V}_{\mathrm{S}}\right)$ |  | 4 to 12 |  | V |
| - $\mathrm{V}_{\mathrm{b}}$ |  |  | 0 to -12 |  | V |
| $+\mathrm{V}_{\mathrm{b} 1},+\mathrm{V}_{\mathrm{b} 2}$ |  |  | 0 to -12 |  | V |
| Input Voltage (Relative to Gain) |  |  | $\pm 2$ |  | V |

Min/max ratings are based on product characterization and simulation. Individual parameters are tested as noted. Outgoing quality levels are determined from tested parameters.

## Notes:

1. $100 \%$ tested at $25^{\circ} \mathrm{C}$.
2. $\mathrm{SE}=$ Single-Ended.

## Typical Operating Characteristics

$\left(\mathrm{G}=+5 \mathrm{~V} / \mathrm{V}(14 \mathrm{~dB}), \mathrm{R}_{\mathrm{L}}=100 \Omega\right.$ (differential), $\mathrm{T}_{\mathrm{a}}=+25^{\circ} \mathrm{C},+\mathrm{V}_{\mathrm{b} 1}=+\mathrm{V}_{\mathrm{b} 2}=+\mathrm{V}_{\mathrm{S}}=+5 \mathrm{~V},-\mathrm{V}_{\mathrm{b}}=-\mathrm{V}_{\mathrm{S}}=-5 \mathrm{~V}$; unless noted)









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2nd Harmonic Distortion vs. $\mathrm{V}_{\mathrm{o}}$


Single Tone Intercept Point



2 Tone 3rd Order Intermod. Distortion


3rd Harmonic Distortion vs. $V_{0}$




## Typical Operating Characteristics

$\left(\mathrm{G}=+5 \mathrm{~V} / \mathrm{V}(14 \mathrm{~dB}), \mathrm{R}_{\mathrm{L}}=100 \Omega\right.$ (differential), $\mathrm{T}_{\mathrm{a}}=+25^{\circ} \mathrm{C},+\mathrm{V}_{\mathrm{b} 1}=+\mathrm{V}_{\mathrm{b} 2}=+\mathrm{V}_{\mathrm{S}}=+5 \mathrm{~V},-\mathrm{V}_{\mathrm{b}}=-\mathrm{V}_{\mathrm{S}}=-5 \mathrm{~V}$; unless noted)


## Functional Description

The circuit is a differential amplifier with current output and feedback. The simplified schematic is shown in Figure 1. The output impedance is set by the value of the feedback resistors (R3-R6) and the gain of the current mirrors. Amplifier gain is set by R1 and R2. All of these resistors are internal due to the high bandwidth of the amplifier.

The common mode output voltage (both outputs together) can be varied by changing the voltages on $+\mathrm{V}_{\mathrm{b} 1},+\mathrm{V}_{\mathrm{b} 2}$ and $-\mathrm{V}_{\mathrm{b}}$. Making all three voltages more negative (for instance, $+\mathrm{V}_{\mathrm{b}}$ 's change from +5 to +3 , and $-\mathrm{V}_{\mathrm{b}}$ changes from -5 to -7 ) will cause the output common mode level to become more positive. The opposite conditions will cause the output common mode level to become more negative. This can be very useful in driving differential circuits which have an elevated DC common mode input level. See Adjusting Common Mode Output Offset Voltage section for more details.

By varying $+\mathrm{V}_{\mathrm{b} 1}$ and $+\mathrm{V}_{\mathrm{b} 2}$ differentially, the differential output offset can be adjusted. See Trimming Differential Output Offset Voltage for more details.


Figure 1: KH600 Simplified Schematic

## Application Information

## General Description

## Standard Operation:

$$
\begin{aligned}
& +\mathrm{V}_{\mathrm{b} 1}=+\mathrm{V}_{\mathrm{b} 2}=+\mathrm{V}_{\mathrm{s}}=+5 \mathrm{~V} \\
& -\mathrm{V}_{\mathrm{b}}=-\mathrm{V}_{\mathrm{S}}=-5 \mathrm{~V}
\end{aligned}
$$

The KH600 is a 1 GHz differential input/output amplifier constructed using Cadeka's in-house thin film resistor/bipolar transistor technology. A differential signal on the inputs of the KH600 will generate a differential signal at the outputs. If a single ended input signal is applied to IN1 and a fixed voltage to IN2, the KH600 will produce both a differential and commonmode output signal. To achieve the maximum dynamic range, center the inputs halfway between $+\mathrm{V}_{\mathrm{S}}$ and $-\mathrm{V}_{\mathrm{S}}$.

The KH600 includes $50 \Omega$ resistors from each input to ground, resulting in a differential input impedance of $100 \Omega$. Each KH600 output has a $50 \Omega$ resistance, synthesized by feedback, providing a $100 \Omega$ differential output impedance.

The KH600 has 3 bias voltage pins that can be used to:

- Adjust the supply current
- Trim the differential output offset voltage
- Adjust the common mode output offset voltage over a $\pm 3 \mathrm{~V}$ range

If these adjustments are not required, short $+\mathrm{V}_{\mathrm{b} 1}$ and $+\mathrm{V}_{\mathrm{b} 2}$ to $+\mathrm{V}_{\mathrm{S}}$ and $-\mathrm{V}_{\mathrm{b}}$ to -Vs as shown in Figure 2. Throughout this data sheet, this configuration $\left(+\mathrm{V}_{\mathrm{b} 1}=+\mathrm{V}_{\mathrm{b} 2}=+\mathrm{V}_{\mathrm{S}}=+5 \mathrm{~V}\right.$ and $-\mathrm{V}_{\mathrm{b}}=-\mathrm{V}_{\mathrm{S}}=-5 \mathrm{~V}$ ) is referred to as the Standard Operating Condition. All of the plots in the Typical Performance section and the specifications in the Electrical Characteristics table utilize the basic circuit configuration shown in Figure 2, unless otherwise indicated. Figure 3 illustrates the optional circuit configuration, utilizing the bias voltage pins. Further discussions regarding these optional adjustments are provided later in this document.


Figure 2: Basic Circuit Configuration


Figure 3: Optional Circuit Configuration (including optional supply current and offset adjust)

## Gain

Differential Gain for the KH600 is defined as (OUT1- OUT2)/ (IN1-IN2). Applying identical (same phase) signals to both inputs and measuring one output will provide the Common Mode Gain. Figure 4 shows the differential and common mode gains of the KH600. Figure 5 illustrates the response of the KH600 outputs when one input is driven and the other is terminated into $50 \Omega$.


Figure 4: Differential and Common Mode Gain


Figure 5: Gain with Single-Ended Input Applied to IN1

## Supply Current

The KH600 draws supply current from the $2 \mathrm{~V}_{\mathrm{s}}$ pins as well as the $3 \mathrm{~V}_{\mathrm{b}}$ pins. Under Standard Conditions, the total supply current is typically 89 mA . Changing the voltages on the bias voltage pins will change their respective supply currents as shown in Figures 6 and 7


Figure 6: $\mathrm{V}_{\mathrm{b}}$ Supply Currents vs. $+\mathrm{V}_{\mathrm{b} 1}$
Changing the voltage on the +Vb 1 pin will alter the supply current for $+\mathrm{V}_{\mathrm{b} 1}$ only, $+\mathrm{V}_{\mathrm{b} 2}$ and $-\mathrm{V}_{\mathrm{b}}$ stay constant at typically 11 mA and 22 mA respectively. See Figure 6 . The same principle applies for $+\mathrm{V}_{\mathrm{b} 2}$. And Figure 7 illustrates the effect of changing $-\mathrm{V}_{\mathrm{b}}$.


Figure 7: $\mathbf{V}_{\mathrm{b}}$ Supply Currents vs $-\mathbf{V}_{\mathrm{b}}$

## Power Dissipation

The KH600 runs at "constant" power, which may be calculated by $\left(\right.$ Total $\left.\mathrm{I}_{\mathrm{S}}\right)\left(\mathrm{V}_{\mathrm{S}}-\left(-\mathrm{V}_{\mathrm{S}}\right)\right)$. Under standard operating conditions, the power is 890 mW . The power dissipated in the package is completely constant, independent of signal level. In other words, the KH600 runs class A.

## Power Supply Rejection Ratio (PSRR)

The KH600 has 5 supply pins, $+\mathrm{V}_{\mathrm{S}},-\mathrm{V}_{\mathrm{S}},+\mathrm{V}_{\mathrm{b} 1},+\mathrm{V}_{\mathrm{b} 2}$, and $-\mathrm{V}_{\mathrm{b}}$. All of these sources must be considered when measuring the PSRR. Figure 8 shows the response of $+\mathrm{V}_{\mathrm{S}}$ and $-\mathrm{V}_{\mathrm{S}}$, looking at OUT2. $+\mathrm{V}_{\mathrm{S}}$ and $-\mathrm{V}_{\mathrm{S}}$ have the same effect on OUT1.


Figure 8: $\pm \mathrm{V}_{\mathbf{s}}$ PSRR
Figure 9 shows the response of OUT1 and OUT2 when $+\mathrm{V}_{\mathrm{b} 1}$ changes. The PSRR of the $\mathrm{V}_{\mathrm{b}}$ pins is "bad", which means that they have a large effect on the response of the KH600 when their voltages are changed. This is the desired effect of the bias voltage pins. As Figure 9 indicates, changing $+\mathrm{V}_{\mathrm{b} 1}$ has a greater effect on OUT1 than it does on OUT2.
Changing $+\mathrm{V}_{\mathrm{b} 1}$ has a direct effect on OUT1. Changing $+\mathrm{V}_{\mathrm{b} 2}$ has a direct effect on OUT2. See the Trimming Differential Output Offset Voltage section for more details.


Figure 9: $+\mathrm{V}_{\mathrm{b}}$ PSRR

## Single-to-Differential Operation

The KH600 is specifically designed for differential-todifferential operation. However, the KH600 can be used in a single-to-differential configuration with some performance degradation. The unused input should be terminated into $50 \Omega$. When driven single-ended, there will be a slight imbalance in the differential output voltages, see Figure 5. This imbalance is approximately 2.88 dB . To compensate for this imbalance, attenuate the higher gain output. (If the signal is applied to IN1, attenuate OUT1.)

## Unused Inputs and/or Outputs

For optimal performance, terminate any unused inputs and/or outputs with $50 \Omega$.

## Adjusting Supply Current

The KH600 operates class A, so maximum output current is directly proportional to supply current. Adjusting the voltages on $+\mathrm{V}_{\mathrm{b} 1}$ and $+\mathrm{V}_{\mathrm{b} 2}$ in opposition to $-\mathrm{V}_{\mathrm{b}}$ controls supply current. The default supply current of the KH600 has been optimized for best bandwidth and distortion performance. The main reason for adjusting supply current is to either reduce power or increase maximum output current. Adjusting the supply current will not significantly improve bandwidth or distortion and may actually degrade them.

To adjust the supply current, apply voltages of equal magnitude, but opposite polarity, to the bias voltage pins. For example, setting $+\mathrm{V}_{\mathrm{b} 1},+\mathrm{V}_{\mathrm{b} 2}$ to +5 VDC and $-\mathrm{V}_{\mathrm{b}}$ to -5 VDC (as shown in Figure 3) results in the standard supply current condition. Setting $+\mathrm{V}_{\mathrm{b} 1},+\mathrm{V}_{\mathrm{b} 2}$ to +5.5 V and $-\mathrm{V}_{\mathrm{b}}$ to -5.5 V results in an approximate $10 \%$ increase in supply current. Figure 10 shows the how the total supply current of the KH600 is effected by changes in the bias voltages $\left(\mathrm{V}_{\mathrm{b}}=+\mathrm{V}_{\mathrm{b} 1}=+\mathrm{V}_{\mathrm{b} 2}=\left|-\mathrm{V}_{\mathrm{b}}\right|\right)$.


Figure 10: Total Supply Current vs. $\mathbf{V}_{\mathbf{b}}$

Supply current is relatively independent of the voltages on $+\mathrm{V}_{\mathrm{S}}$ and $-\mathrm{V}_{\mathrm{S}}$ as shown in Figure 11.


Figure 11: Total Supply Current vs. $\mathbf{V}_{\mathbf{S}}$


Figure 12: -3dB Bandwidth vs. Is


Figure 13: Harmonic Distortion vs. Total $\mathrm{I}_{\mathrm{s}}$


Figure 14: Harmonic Distortion vs. Total $I_{s}$

## Trimming Differential Output Offset Voltage

Vary $+\mathrm{V}_{\mathrm{b} 1}$ and $+\mathrm{V}_{\mathrm{b} 2}$ to adjust differential offset voltage. $+\mathrm{V}_{\mathrm{b} 1}$ controls OUT1 and $+\mathrm{V}_{\mathrm{b} 2}$ controls OUT2. The output voltage moves in a direction opposite to the direction of the bias voltage. Figure 15 shows the resulting voltage change at OUT1 and OUT2 when the voltage on $+\mathrm{V}_{\mathrm{b} 1}$ is changed. Figure 16 shows the resulting voltage change at OUT1 and OUT2 when the voltage on $+\mathrm{V}_{\mathrm{b} 2}$ is changed. OUT1 and OUT2 change at the same rate when -Vb is changed, as shown in Figure 17. Therefore, changing the voltage on $-\mathrm{V}_{\mathrm{b}}$ has no effect on differential output offset voltage.


Figure 15: Output vs. $+\mathrm{V}_{\mathrm{b} 1}$


Figure 16: Output vs. $+\mathrm{V}_{\mathrm{b} 2}$


Figure 17: Output vs. $-\mathrm{V}_{\mathrm{b}}$

## Adjusting Common Mode Output Offset Voltage

Short $+\mathrm{V}_{\mathrm{b} 1}$ to $+\mathrm{V}_{\mathrm{b} 2}$ and vary $+\mathrm{V}_{\mathrm{b}}$ and $-\mathrm{V}_{\mathrm{b}}$ to adjust common mode output offset voltage. The recommended values for achieving a given output offset are shown in Figure 18. These values were chosen to give the best distortion performance. The exact values are not crucial.


Figure 18: $\mathrm{V}_{\mathrm{b}}$ vs. Common Mode Voltage
For common mode voltages of 0 to -3.5 V swap the $\mathrm{V}_{\mathrm{b}}$ 's and change the polarity. See the example below.

| Desired Common <br> Mode Voltage | $+\mathbf{V}_{\mathrm{b} 1}$ and $+\mathrm{V}_{\mathrm{b} 2}(\mathrm{~V})$ | $-\mathbf{V}_{\mathrm{b}}(\mathrm{V})$ |
| :---: | :---: | :---: |
| 2 Volts | 2 | -8 |
| -2 Volts | 8 | -2 |

Figures 19 and 20 illustrate how the common mode voltage effects harmonic distortion. Figure 21 shows the resulting $I_{S}$ and $-I_{S}$ supply currents.

Pay close attention to your peak-to-peak output voltage requirement. As you change the common mode voltage, you may need to increase or shift $\pm V_{S}$ in order to achieve your output requirements. A 2 V margin is recommended. For example, if your output requirement is $5 \mathrm{~V}_{\mathrm{pp}}$ and you will be
changing the common mode from 1 V to 3 V set $\mathrm{V}_{\mathrm{S}}=+7.5$ and $-\mathrm{V}_{\mathrm{S}}$ to -3.5 V . This example calls for a supply voltage of greater than 10V. This will not effect supply current because as Figure 11 indicates, changing $\pm \mathrm{V}_{\mathrm{S}}$ has no effect on supply current.


Figure 19: $2 \mathrm{~V}_{\mathrm{pp}} \mathrm{HD}$ vs. Common Mode Voltage


Figure 20: $5 \mathrm{~V}_{\mathrm{pp}} \mathrm{HD}$ vs. Common Mode Voltage


Figure 21: Resulting $\mathrm{I}_{\mathrm{s}}$ and $-\mathrm{I}_{\mathbf{s}}$

## Layout Considerations

General layout and supply bypassing play major roles in high frequency performance. Cadeka has evaluation boards to use as a guide for high frequency layout and as aid in device testing and characterization. Follow the steps below as a basis for high frequency layout:

- Include all recommended $6.8 \mu \mathrm{~F}$ and $0.01 \mu \mathrm{~F}$ bypass capacitors
- Place the $6.8 \mu \mathrm{~F}$ capacitors within 0.75 inches of the power pin
- Place the $0.01 \mu \mathrm{~F}$ capacitors within 0.1 inches of the power pin
- Remove the ground plane under and around the part, especially near the input and output pins to reduce parasitic capacitance
- Minimize all trace lengths to reduce series inductances
- A 10 pF to 50 pF bypass capacitor can be used between pins 5 and 6 and between pins 10 and 11 to reduce crosstalk from the positive supply

Refer to the evaluation board layouts shown in Figure 22 for more information.

## Evaluation Board Information

The following evaluation boards are available to aid in the testing and layout of this device:

| Evaluation <br> Board | Description | Products |
| :---: | :--- | :---: |
| KEB007 | Basic KH600 Eval Bd | KH600 |
| KEB009 | KH600 Eval Bd with offset and <br> $\mathrm{I}_{\text {cc }}$ Adjust Option | KH600 |

Do not include capacitors C2, C3, C7, C11, and C12 that are shown on the KEB007 evaluation board. Evaluation board schematics and layouts are shown in Figure 22. Refer to the schematic shown in Figure 1 for the KEB007 board and Figure 3 for the KEB009 board.

## KH600 Evaluation Board Layout



Figure 22a: KEB007 (top side)


Figure 22c: KEB009 (top side)


Figure 22b: KEB007 (bottom side)


Figure 22d: KEB009 (bottom side)

## Ordering Information

| Model | Part Number | Package | Evaluation Board |
| :---: | :---: | :---: | :---: |
| KH600 | KH600AI | 12-pin TO8 | KEB007, KEB009 |

Temperature range: $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$.

## KH600 Package Dimensions



| TO-8 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| SYMBOL | INCHES |  | MILIMETERS |  |
|  | Minimun | Maximum | Minimum | Maximum |
| A | 0.142 | 0.181 | 3.61 | 4.60 |
| ¢b | 0.016 | 0.019 | 0.41 | 0.48 |
| $\phi \mathrm{D}$ | 0.595 | 0.605 | 15.11 | 15.37 |
| $\phi D_{1}$ | 0.543 | 0.555 | 13.79 | 14.10 |
| e | 0.400 BSC |  | 10.16 BSC |  |
| $\mathrm{e}_{1}$ | 0.200 BSC |  | 5.08 BSC |  |
| $\mathrm{e}_{2}$ | 0.100 BSC |  | 2.54 BSC |  |
| F | 0.016 | 0.030 | 0.41 | 0.76 |
| k | 0.026 | 0.036 | 0.66 | 0.91 |
| $\mathrm{k}_{1}$ | 0.026 | 0.036 | 0.66 | 0.91 |
| L | 0.310 | 0.340 | 7.87 | 8.64 |
| $\alpha$ | $45^{\circ} \mathrm{BSC}$ |  | $45^{\circ} \mathrm{BSC}$ |  |

## NOTES:

Seal: cap weld
Lead finish: gold per MIL-M-38510 Package composition: Package: metal Lid: Type A per MIL-M-38510

## Life Support Policy

Cadeka's products are not authorized for use as critical components in life support devices or systems without the express written approval of the president of Cadeka Microcircuits, Inc. As used herein:
 in accordance with instructions for use provided in the labeling, can be reasonably expected to result in a significant injury to the user.
2. A critical component is any component of a life support device or system whose failure to perform can be reasonably expected to cause the failure of the life support device or system, or to affect its safety or effectiveness.
Cadeka does not assume any responsibility for use of any circuitry described, and Cadeka reserves the right at any time without notice to change said circuitry and specifications.

